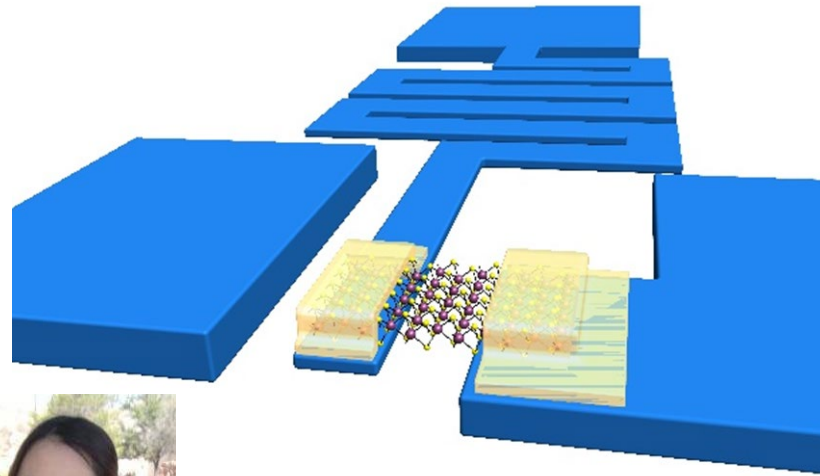


# Stritch Research Update



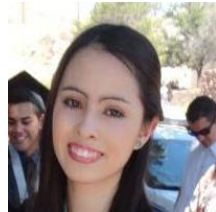
## UTEP TEAM:



David  
Zubia



Aldo  
Vidana



Mariana  
Martinez



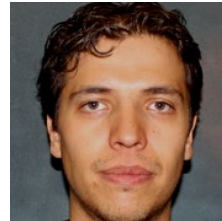
Edgar  
Acosta



Raquel  
Zubia

## COLLABORATORS:

UCB



Dr. Sergio  
Almeida

UCB



Dr. Tsu-Jae  
King Liu

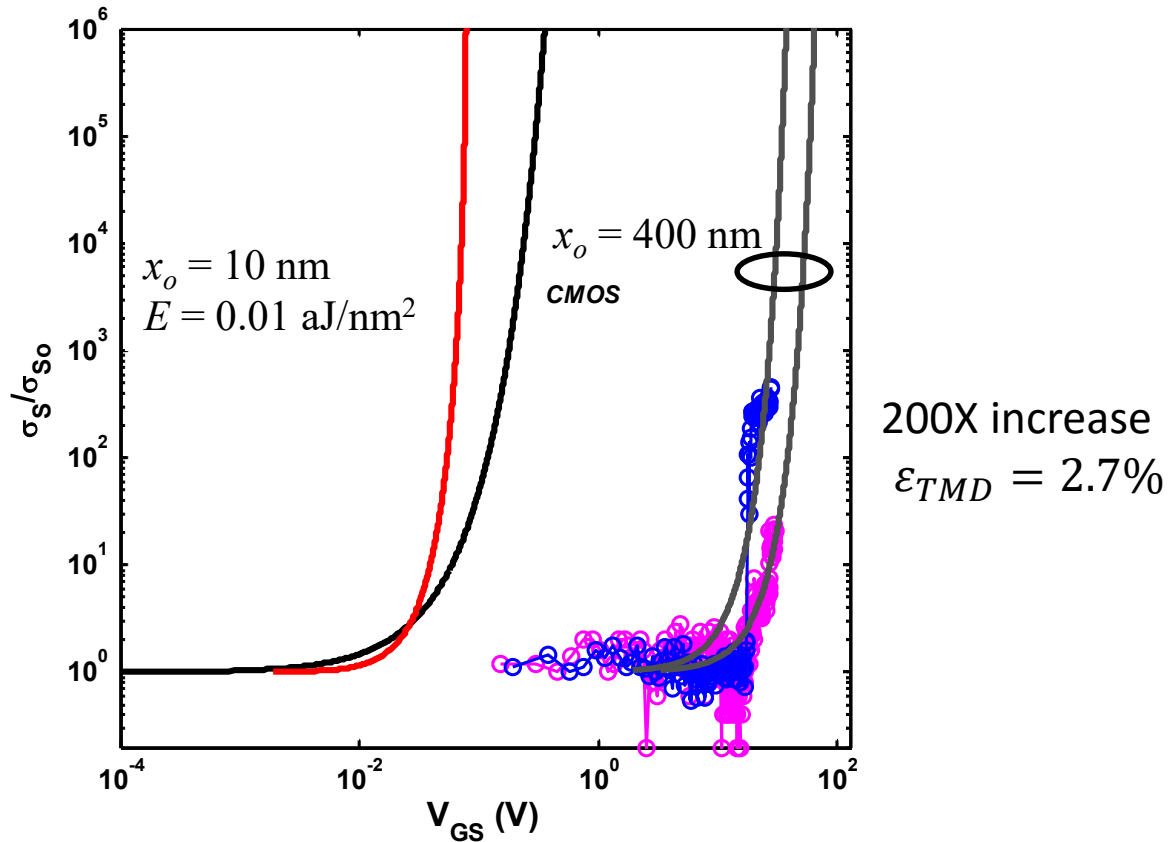
UACJ-Mexico



Dr. Jose  
Mireles



# Stritch Output Characteristic



➤ **Swing<sub>Stritch</sub> (17mV/dec) < Swing<sub>CMOS</sub> (60 mV/dec)**



# Stritch Output Characteristic

- What gives rise to steep output?
- How can steep output be used?

**CMOS:**  $\sigma_{CMOS}/\sigma_{CMOS_0} = \exp(V_{GS}/kT)$

**Stritch:**  $\sigma_S/\sigma_{S_0} = \exp\left(\left|\frac{\partial E_g}{\partial \varepsilon}\right| \varepsilon(V_{GS})/2kT\right)$

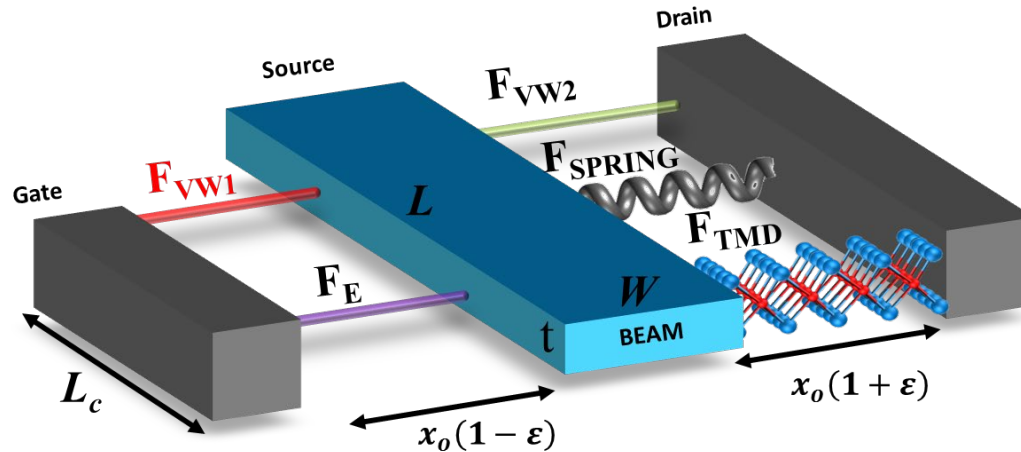
TMD deformation potential      MEMS actuation sensitivity

Stritch output is steeper than CMOS when:

$$\left|\frac{\partial E_g}{\partial \varepsilon}\right| \varepsilon(V_{GS})/2 > 1$$



# MEMS Actuation Sensitivity

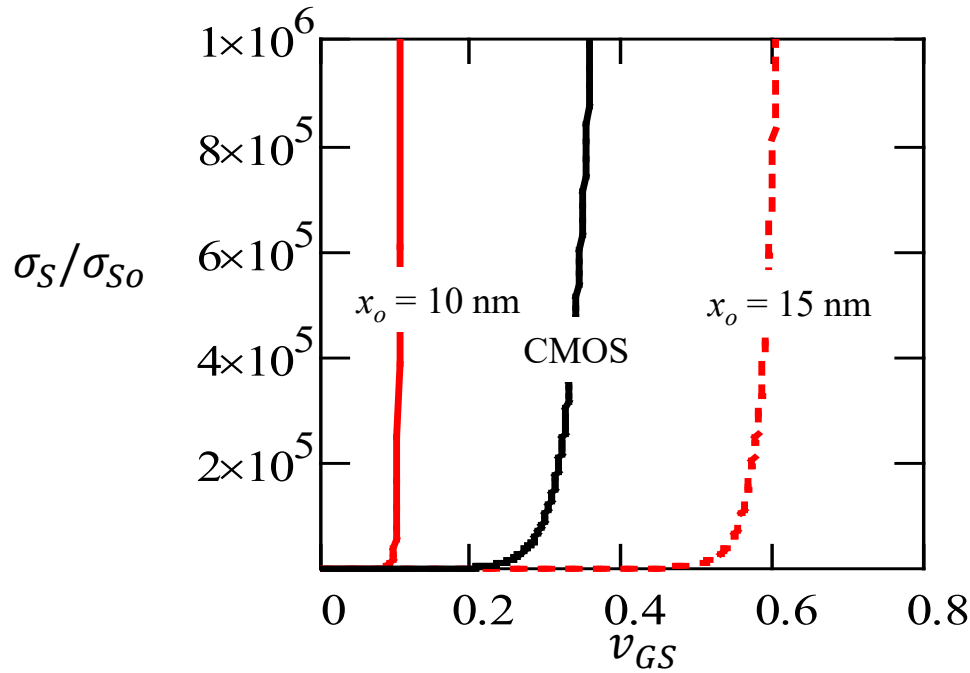
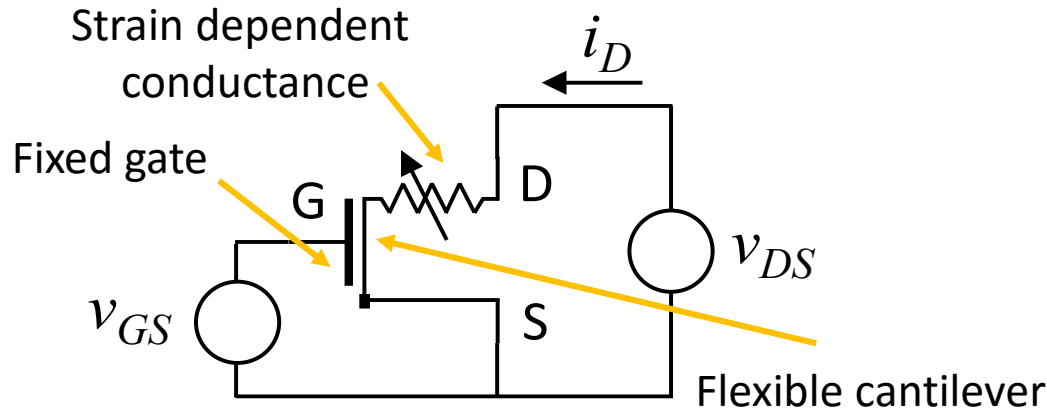


$$F_E = F_{CAN} + F_{TMD} + F_{VW_2} - F_{VW_1}$$

$$\frac{\epsilon_0 A V_{GS}^2}{2x_0^2 (1 - \epsilon)^2} = k_{CAN} x_0 \epsilon + k_{TMD} x_0 \epsilon + \frac{HA}{6\pi x_0^3 (1 + \epsilon)^3} - \frac{HA}{6\pi x_0^3 (1 - \epsilon)^3}$$

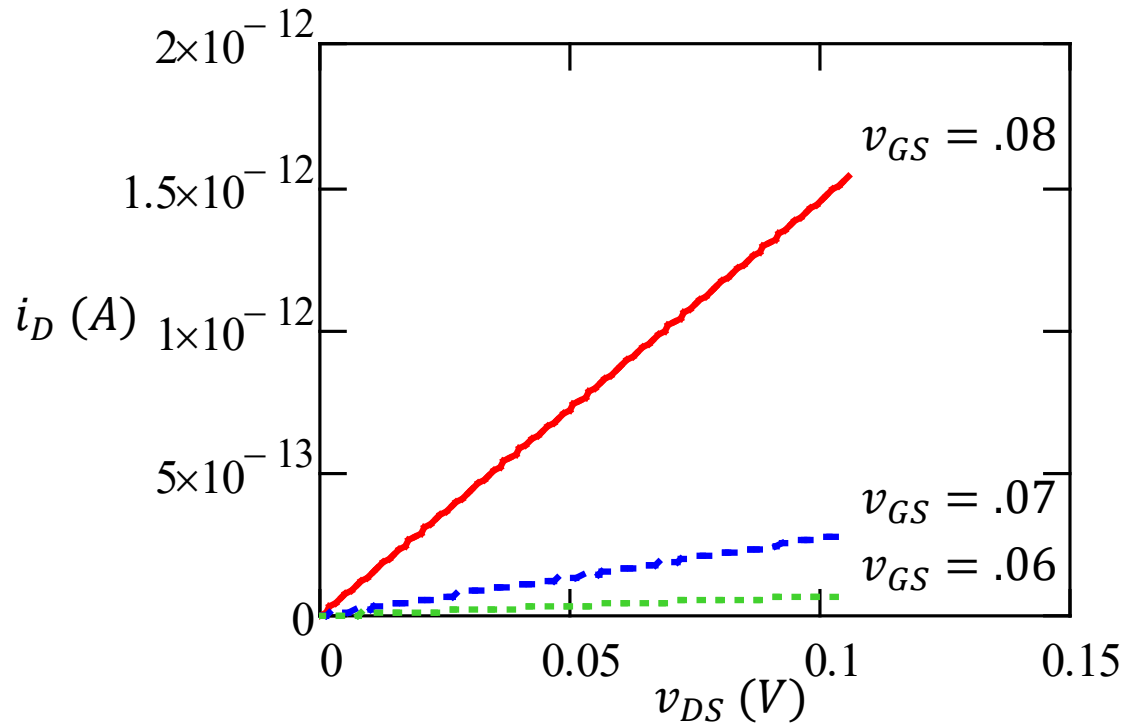
- $F_{VW_1}$  aids  $F_E$  to strain TMD when  $x_0$  is small
- $F_{VW_1}$  increases actuation sensitivity  $\left( \frac{\Delta \epsilon}{\Delta V_{GS}} \right)$

# Stritch Transistor



- Turn-on voltage is sensitive to  $x_0$
- Output remains steep

# I-V Characteristic



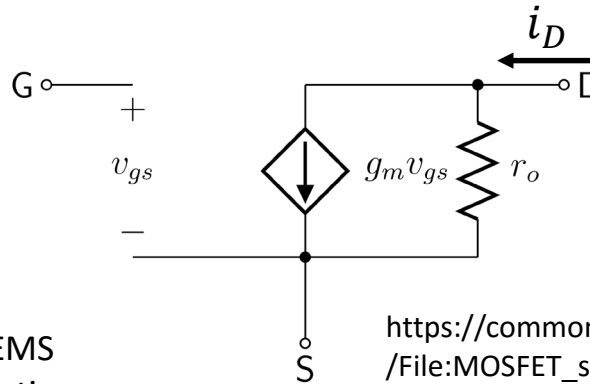
- Similar to MOSFET in linear region
- However slope increases exponentially with  $v_{GS}$



# Stritch Small Signal Model

$$v_{ds} = g_m v_{gs} r_o$$

$$i_d = g_m v_{gs} + v_{ds}/r_o$$



[https://commons.wikimedia.org/wiki/File:MOSFET\\_small\\_signal.svg](https://commons.wikimedia.org/wiki/File:MOSFET_small_signal.svg)

TMD deformation potential

MEMS actuation sensitivity

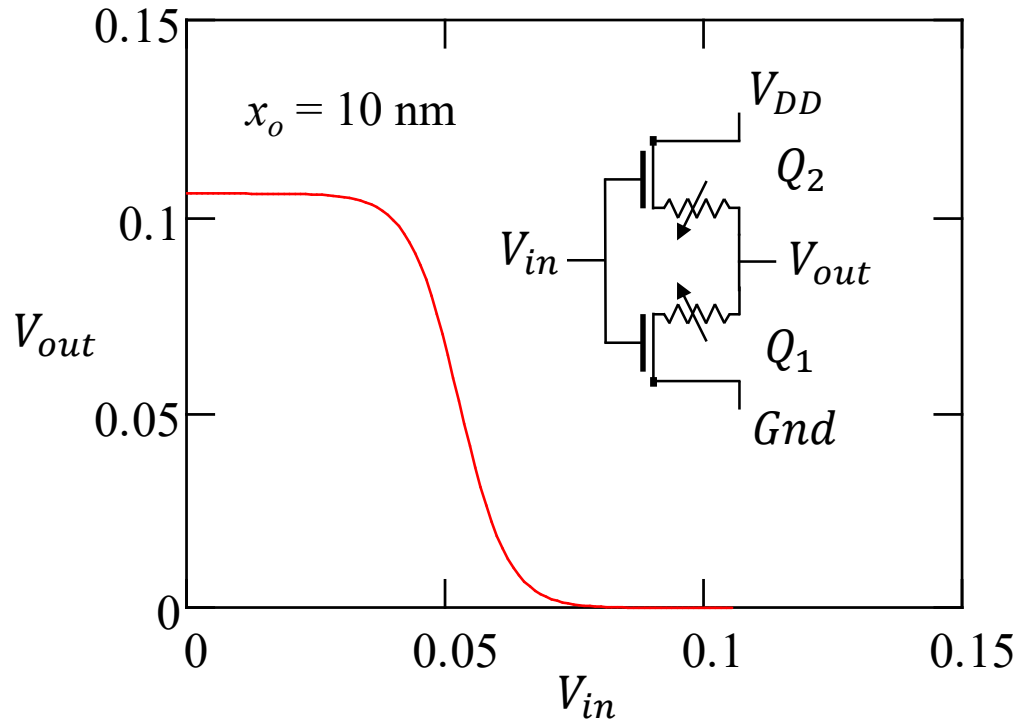
$$g_m \equiv I_{DQ} \frac{\left| \frac{\partial E_g}{\partial \varepsilon} \right| \left( \frac{\partial \varepsilon}{\partial V_{GS}} \right)}{2kT} = V_{DSQ} \sigma_{SQ} \frac{\left| \frac{\partial E_g}{\partial \varepsilon} \right| \left( \frac{\partial \varepsilon}{\partial V_{GS}} \right)}{2kT}$$

$$r_o \equiv \frac{1}{\sigma_{SQ}} = 1 / \sigma_{SQ} \exp \left( \left| \frac{\partial E_g}{\partial \varepsilon} \right| \varepsilon(V_{GSQ}) / 2kT \right)$$

$$A_{Vo} = \frac{v_{ds}}{v_{gs}} = g_m r_o = V_{DSQ} \frac{\left| \frac{\partial E_g}{\partial \varepsilon} \right| \left( \frac{\partial \varepsilon}{\partial V_{GS}} \right)}{2kT}$$

# Complementary Logic Configuration

$$V_{out} = V_{DD} \frac{R_1(V_{in})}{R_1(V_{in}) + R_2(V_{DD} - V_{in})}$$



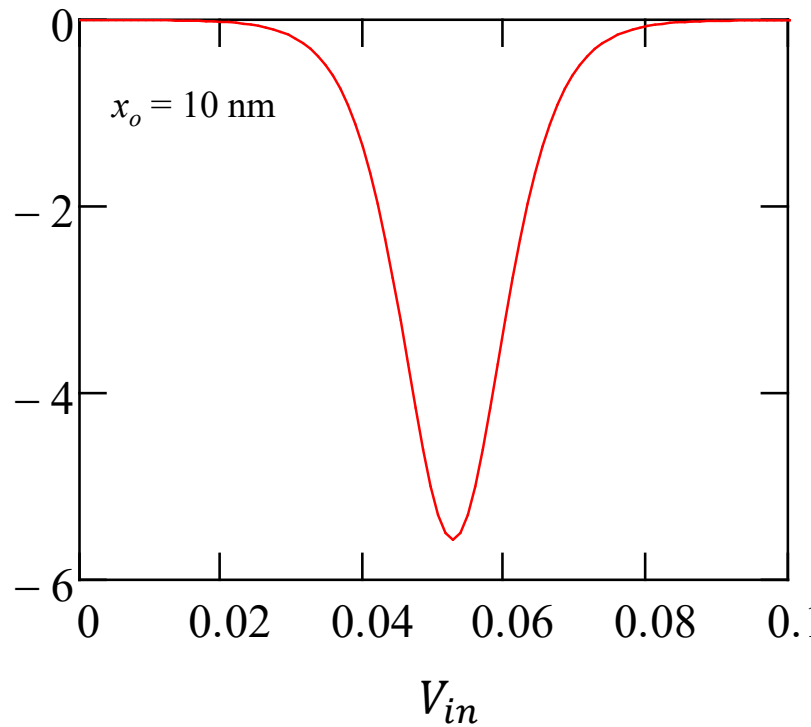
- **Electrostatic force is ambipolar**
  - ❑ **Allows inverting and non-inverting circuitry**





# Voltage Gain of Complementary Circuit

$$A_V = \frac{V_{out}}{V_{in}}$$

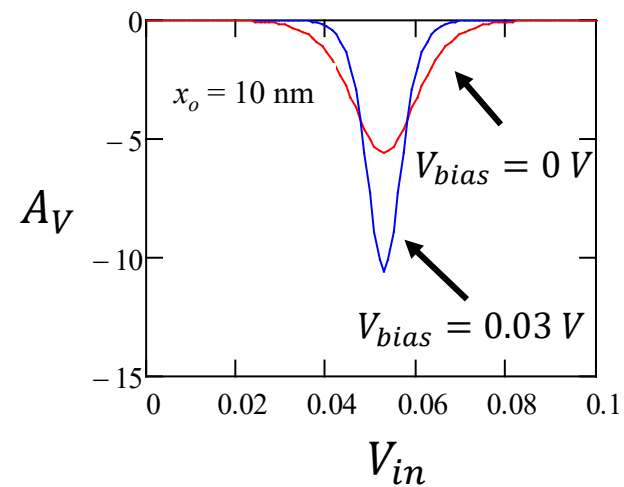
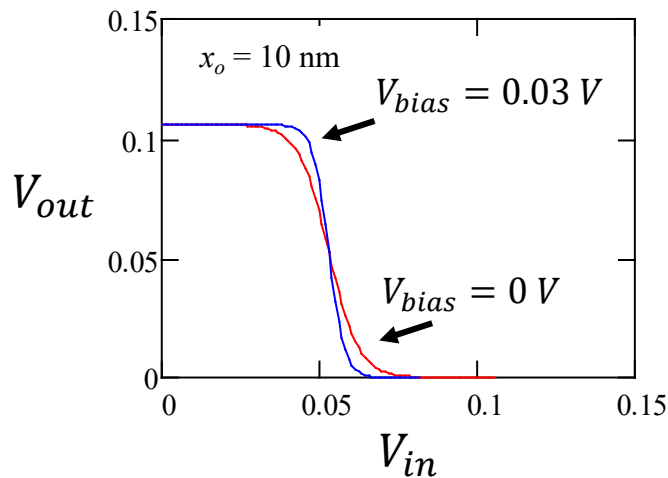
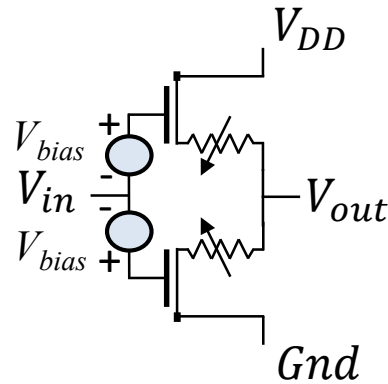


➤ Maximum  $A_V = -5.5$

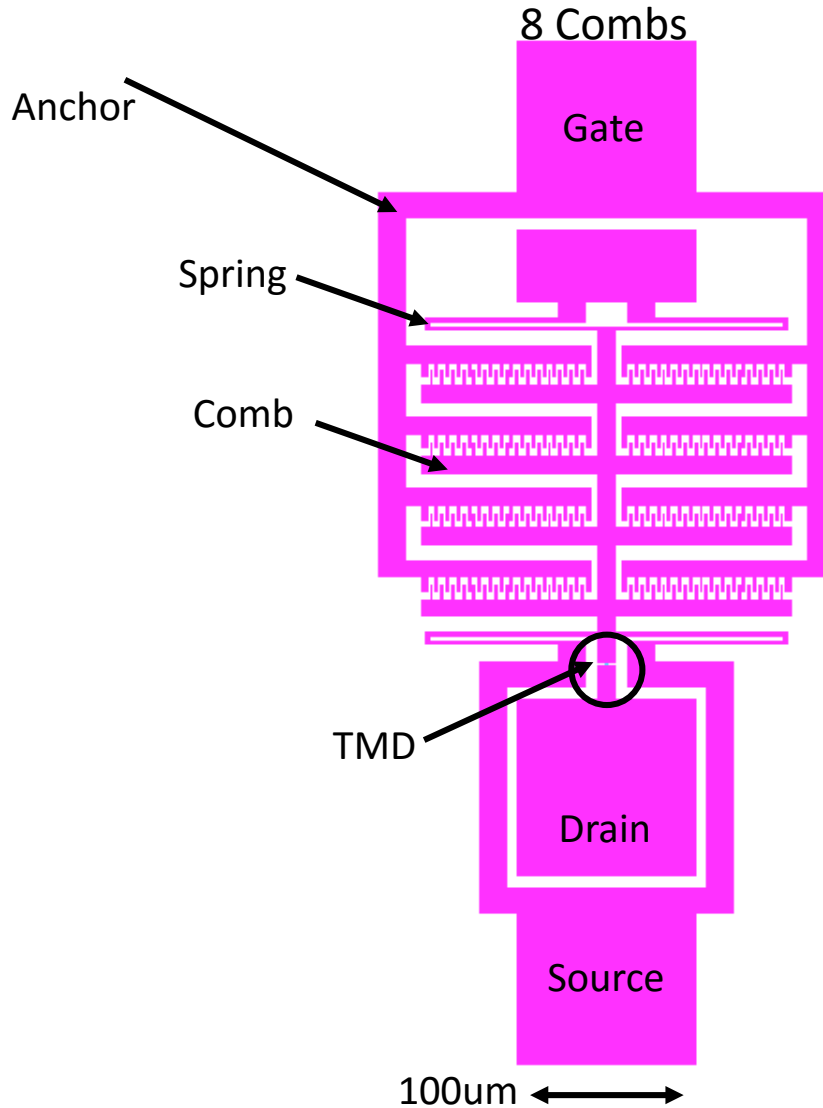


# DC Bias Increases Gain

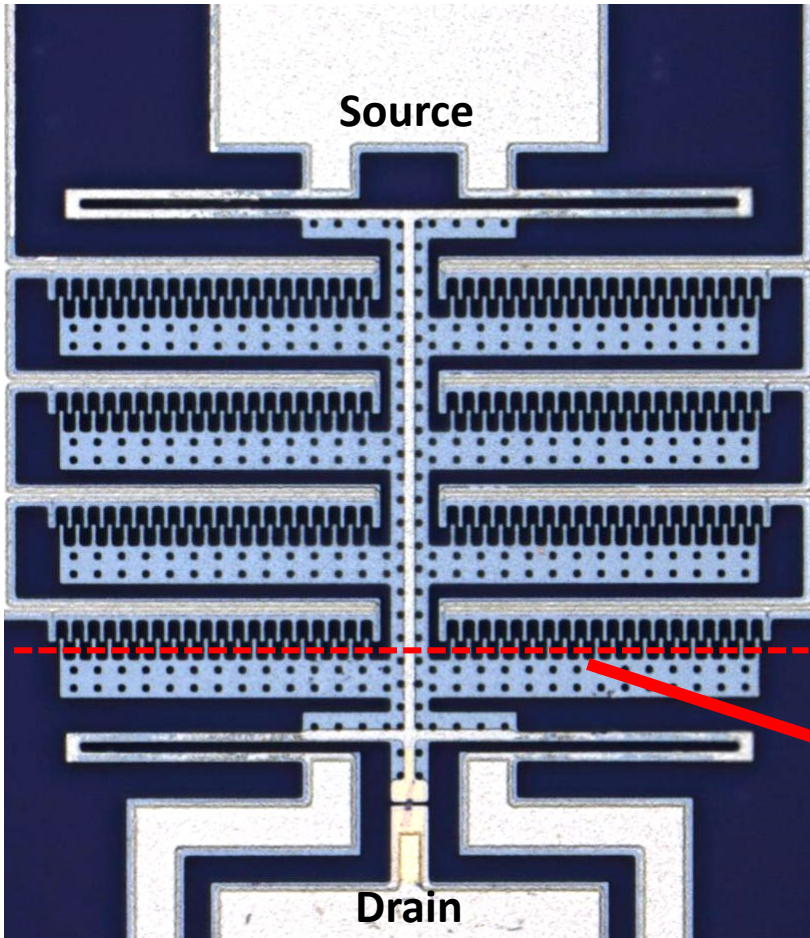
- **Bias pre-actuates MEMS**
  - **Increases actuation sensitivity**



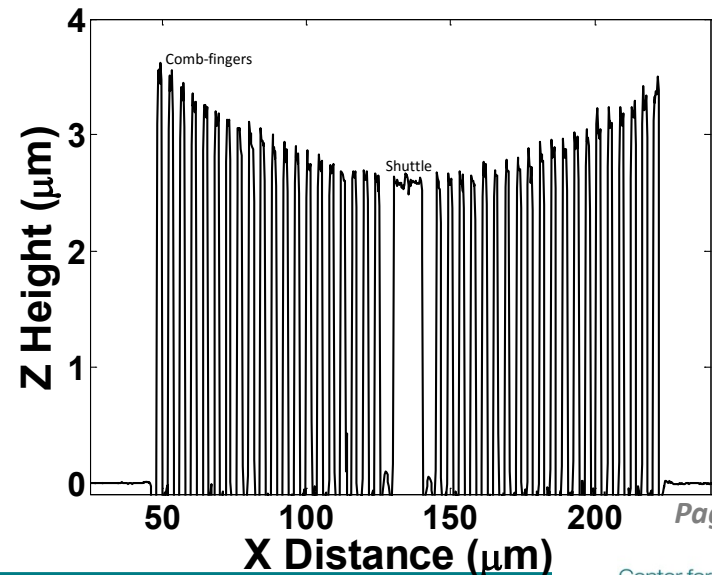
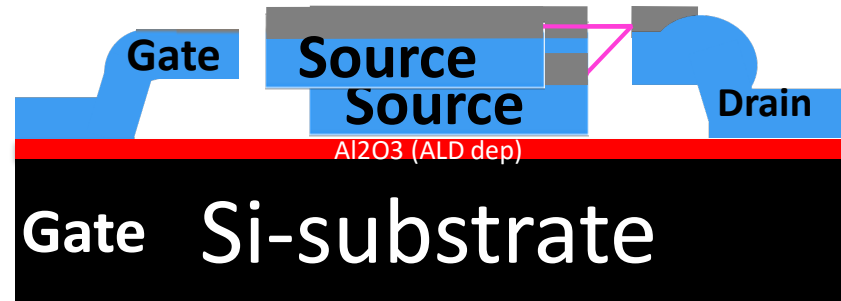
# UTEP Comb-Drive Design



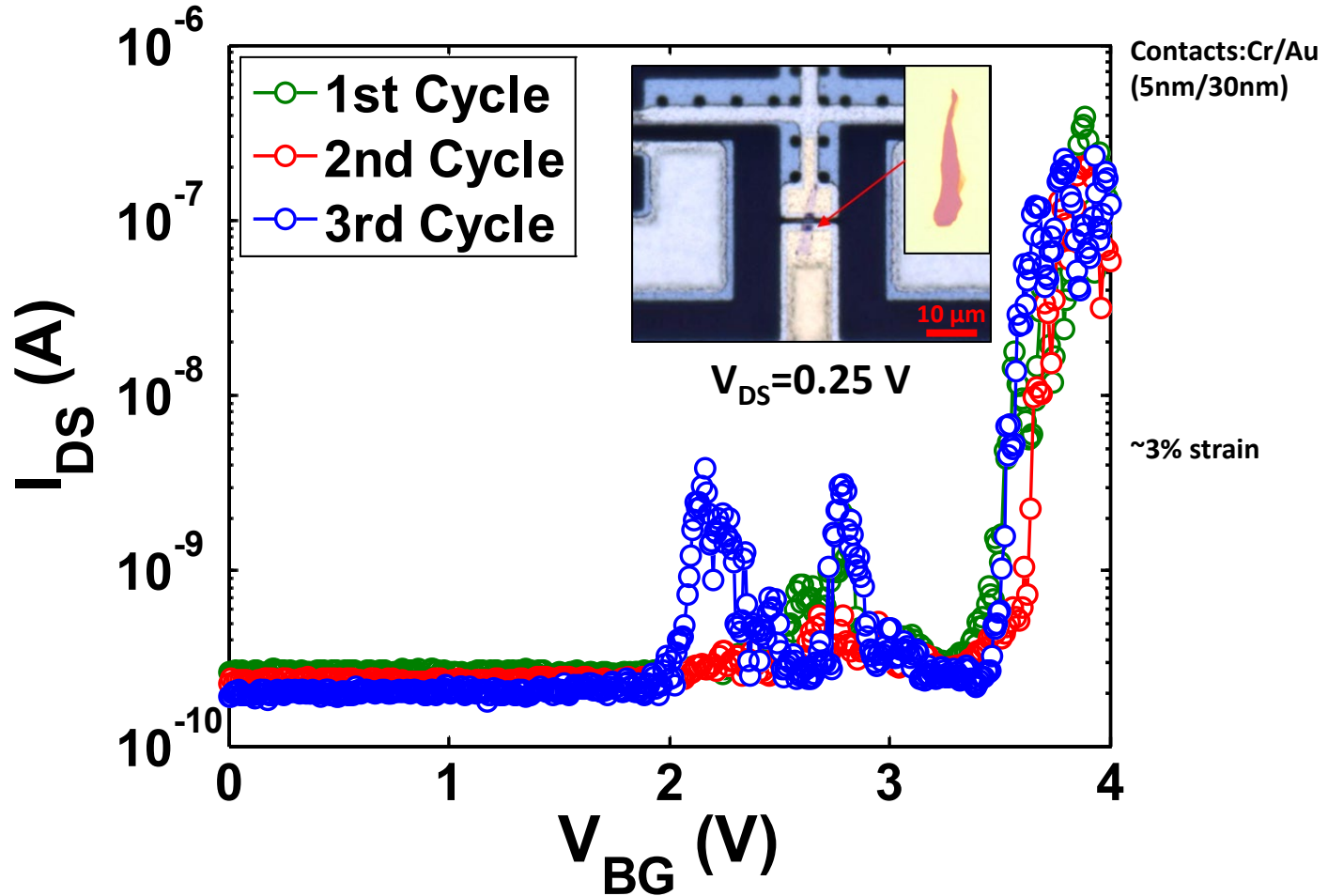
# Lateral vs Vertical Actuation



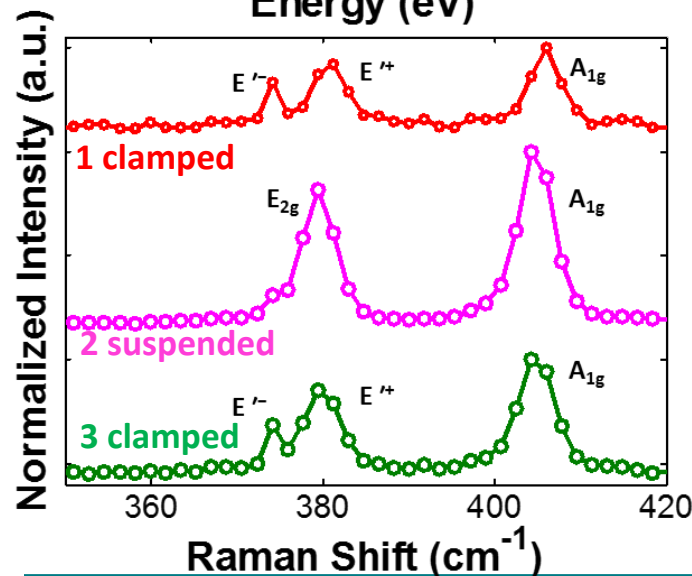
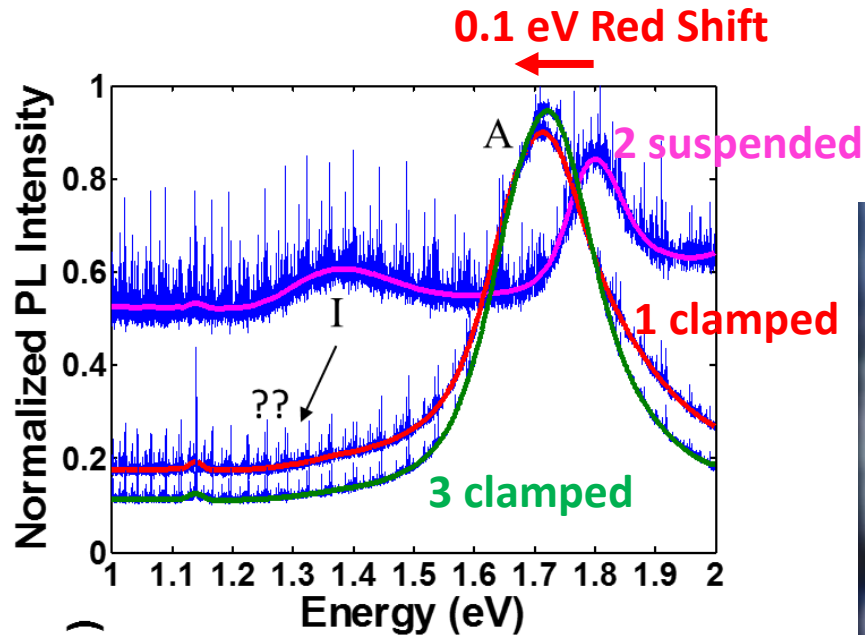
## VERTICAL ACTUATION



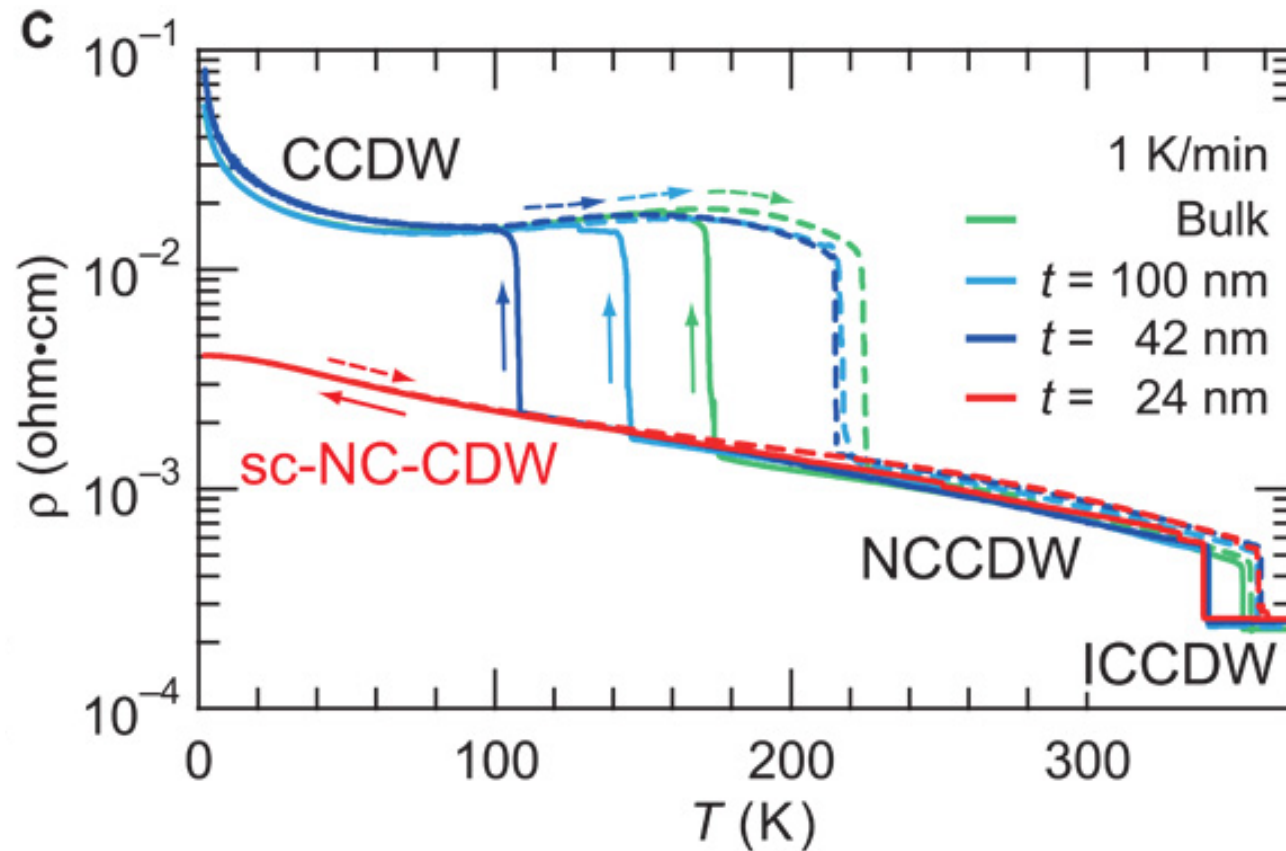
# 3000X increase in conductivity in strained MoS<sub>2</sub>



# Optical measurements after straining



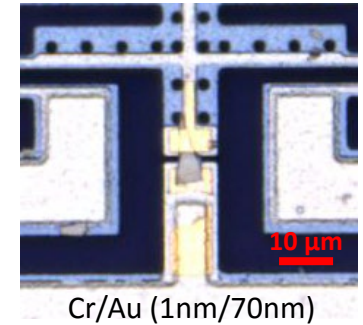
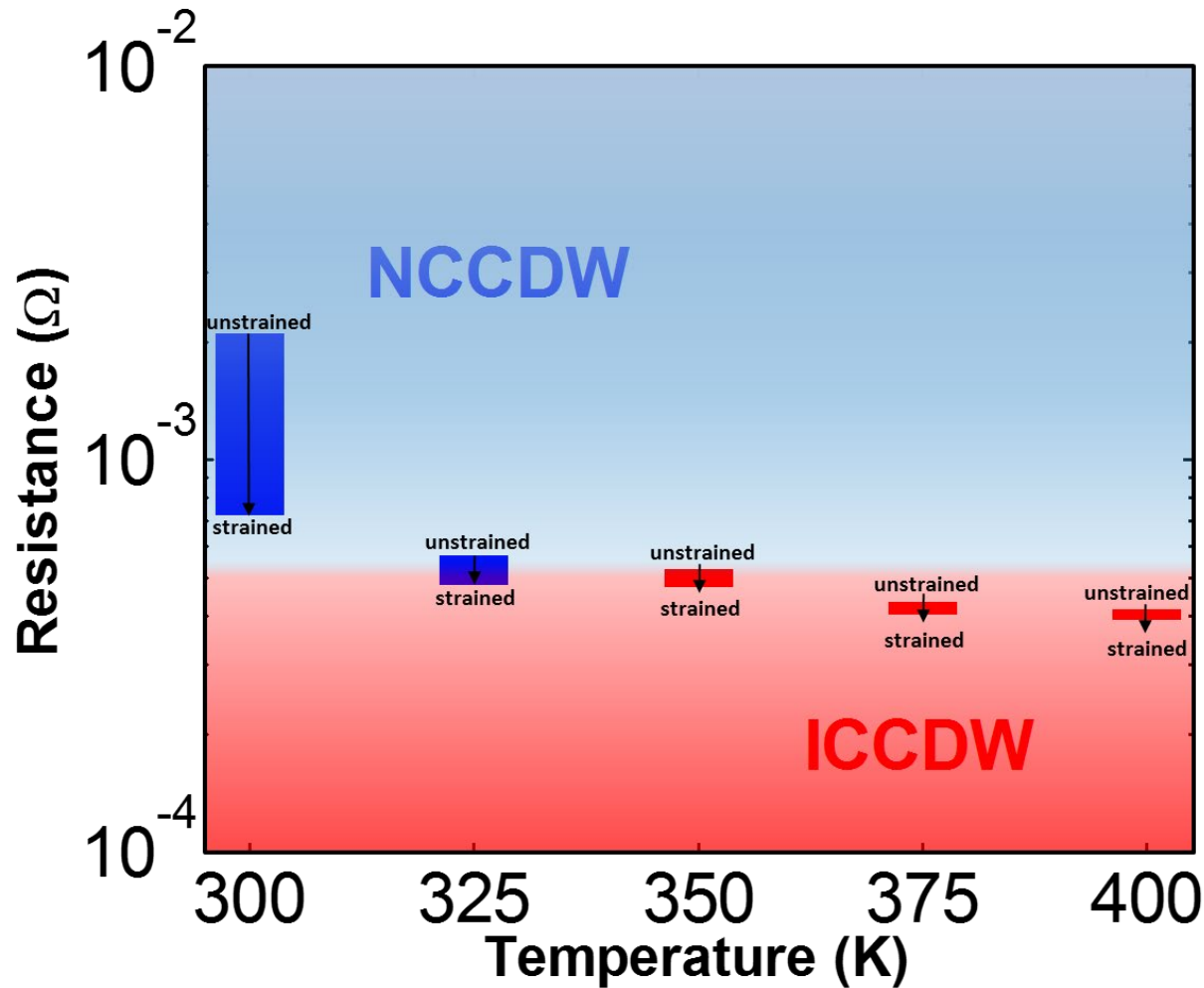
# TaS<sub>2</sub>-layered system with first-order charge density wave (CDW) phase transitions



DOI: 10.1126/sciadv.1500606



# Phase transition temperature shift in strained TaS<sub>2</sub>





# Thank You!

